

某压气机九级盘低循环疲劳寿命试验评估

燃气涡轮研究所 龚梦贤 王旅生 曹凤兰 邓剑波 茹梅秀

1. 某压气机九级盘与试验九级盘 鉴于按照应力疲劳理论给出的名义应力法研究某压气机鼓筒低循环疲劳寿命时得出的结论:九级盘偏心孔部位是限制鼓筒使用寿命的最关键部位。故本文特将基于应变疲劳理论的伴随试验法用于此压气机九级盘低循环疲劳寿命评估。

九级盘在某压气机中的装配关系见图1a。A处装配紧度最大值为0.17mm,最小值为0.07mm。B处装配紧度最大值为0.36mm,最小值为0.18mm。计算结果表明,后轴颈与九级盘之间的装配紧度对九级盘偏心孔处应力的影响远远大于八级盘与九级盘之间装配紧度对九级盘偏心孔处应力的影响。前者大约占95%,后者大约占5%^[1]。故设计的九级盘单盘试验转子中九级盘所带鼓筒的一部分已经切除,八级盘也已取消,后轴颈则由一个既起转接作用(连接九级盘与SB804试验器柔轴),又模拟其刚度的模拟后轴颈所代替(图1b),B处装配紧度保持不变。计算表明,在转速谱相同的情况下,试验转子中的九级盘偏心孔处应力应变历程与原九级盘偏心孔处应力应变历程相同。

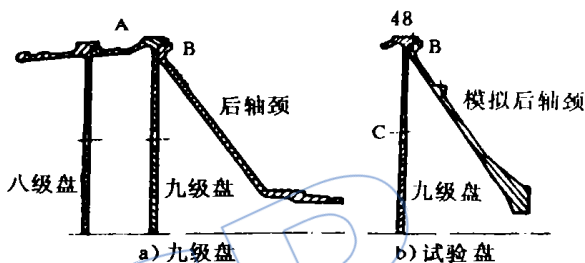


图1 某压气机九级盘 (a 九级盘 b 试验盘)

2. 伴随试验 理论计算与应变实测确定九级盘偏心孔最危险部位(图1b的C处)的应变循环上下限分别为 $7164\mu\epsilon$ 和 $1085\mu\epsilon$ (对应循环上下限转速分别为11850r/min和1600r/min),此即九级盘的应变历程。在此应变历程下做伴随试验的光滑圆棒试样是从九级盘毛坯上取料加工的,其热处理制度与九级盘的完全相同。伴随试验在HS84002低周疲劳试验机上进行。共做了八根试样,其疲劳断裂寿命分别是7500、7977、8227、9336、9631、10312、11310、11410周。按疲劳试验统计分析标准进行统计处理,知此组子样满足存活率99.9%,置信度95%,误差限5%的要求。计算得到伴随试验试样断裂寿命中值为9360周,存活率为99.9%的断裂寿命为5730周。根据文献[2]的结论,此伴随试验预测九级盘偏心孔处低循环疲劳裂纹起始寿命中值为9360周,存活率为99.9%的低循环疲劳裂纹起始寿命为5730周。

3. 九级盘疲劳试验 九级盘疲劳试验在SB804试验器上进行。图1b所示试验转子通过一根柔轴与SB804试验器上刚轴相连,封闭在试验器的真空腔中(图2)。试验转子的循环旋转是由微机自动控制的。试验时每隔一定的循环次数进行着色检查,先后观察到有五条疲劳裂纹贯穿盘厚(图3)。由图3可见,九级盘偏心孔一周不同部位的应变虽有差异,但差异

并不大。这五条裂纹的扩展情况示于图 4。若定义从盘的表面第一次出现 0.8mm 长裂纹时的循环次数为九级盘低循环疲劳裂纹起始寿命 N_0 ，则由图 4 中 3-1[#] 裂纹扩展曲线可以推知 N_0 为 12768 周。若定义盘上裂纹进入失稳扩展时循环次数为盘的疲劳失效寿命 N_f (即总寿命)，则由图 4 可以推知 N_f 约为 20215 周。同时可以推知九级盘裂纹扩展寿命约为 7447 周。亦可推知九级盘低循环疲劳裂纹起始寿命占总寿命的 63%。

对九级盘上出现的五个断口，均进行了用疲劳条带定量反推疲劳裂纹起始寿命的工作。此工作由西北工业大学完成。以盘上最先观察到的 3-1[#] 裂纹为例 (图 2C 处)，断口反推到的穿透裂纹扩展寿命为 7925 周。已知总寿命为 20215 周，则此穿透裂纹的起始寿命 N_0 为 12290 周。由于裂纹在未穿透前沿盘厚还有一段扩展寿命，若定义表面裂纹宽度为 0.8mm 时的循环次数为此疲劳裂纹起始寿命 N_0 ，则经断口反推到的 N_0 为 9806 周。

4. 对比与结论 实验时宏观观测到 $N_0 = 12768$ 周与通过断口疲劳条带定量反推得到 $N_0 = 12290$ 周基本吻合。伴随试验所预测的九级盘偏心孔处低循环疲劳裂纹起始寿命中值 9360 周与通过断口疲劳条带定量反推得到的 $N_0 = 9806$ 周，同样是基本吻合。即使将伴随试验所预测的疲劳裂纹起始寿命中值 9360 周与实验时宏观观测到的 $N_0 = 12768$ 周相比较，二者也是接近的，预测误差在 30% 以内。

由此可得出结论：

(1) 图 2 所示九级盘单盘低循环疲劳试验是成功的，再现了某压气机鼓筒低循环疲劳时九级盘偏心孔处疲劳裂纹的起裂位置、走向及其扩展规律；

(2) 伴随试验法^[2]对于实际型号盘的低循环疲劳裂纹起始寿命的试验评估是有效的。

参 考 文 献

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- [2] 王旅生、龚梦贤、梁彩容、茹梅秀，‘轮盘偏心孔低循环疲劳寿命预测法’，航空动力学报，第 3 卷，第 2 期，1988 年 4 月。

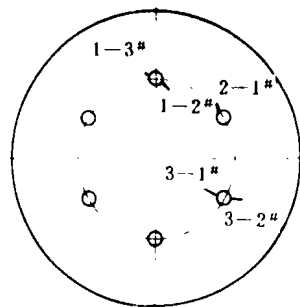
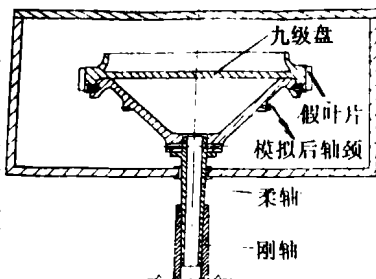


图 2 安装在试验器上的九级盘试验转子 图 3 九级盘穿透裂纹的位置及走向

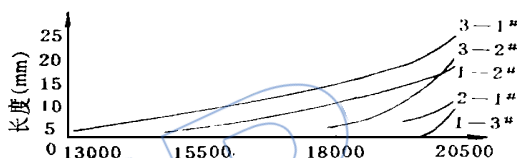


图 4 九级盘穿透裂纹扩展曲线

crack initiation is 8642 (cycles). In comparison with cyclic rotating tests, the test period on a multi-channel radial loading fatigue test rig can be shortened greatly and the test data can be obtained easily. A smooth round bar specimen experiment method for predicting the LCF life of groove bottom in the disk is provided, which is better than the Morrow method. For the median LCF life, the ratio of the experimental life to the predicted life is 1.2.

EXPERIMENTAL ESTIMATION OF LCF LIFE FOR A COMPRESSOR DISK

Gong Mengxian, Wang Lusheng, Cao Fenglan, Ru Meixiu
(*Gas Turbine Establishment*)

ABSTRACT A LCF (Low Cycle Fatigue) test of a single rotor disk of a compressor is presented. The experimental results show that the location and the growth orientation of LCF crack in 9th single rotor disk reproduce those in the global compressor rotor. In addition, the LCF tests of the smooth round bar specimens are accompanied with the LCF tests of a single rotor disk, so as to estimate of the strain history of the eccentric holes in the disk. The statistical data of smooth round bar specimens tested to failure enables to estimate the LCF life to crack initiation for the eccentric holes in the disk of the global compressor rotor.

AN EXPERIMENTAL STUDY ON DISC BURSTING SPEED

Zheng Qixuan

(*Beijing University of Aeronautics and Astronautics*)

ABSTRACT This paper describes the experimental work on the research of disc bursting speed. The bursting speed tests for a series of disc models are made successfully. That means: such a difficult experimental technique has been mastered; and the reconstructed horizontal test rig is suitable for the research of disc bursting speed at normal atmospheric temperature and with heating. The results obtained from experiments and calculations are coincident. This work provides the basis for the further research on the bursting speed of aeroengine discs.

MODIFICATION OF SHAPE OF DOVETAIL JOINTS FOR ANTI-FRETTING DAMAGE

Zhu Rupeng, Pan Shengcai, Dai Zhendong
(*Nanjing Aeronautics Institute*)

ABSTRACT The fretting damage of the dovetail joints between blades and disks in turbojet engines has significant effect on fatigue life of the joints. In order to improve the resistibility to of dovetail joints fretting damage, an effective method provided, which palliates the fretting wear of the joint. By modifying the shape of the local interface to adjust the distribution of the mechanical parameters. The numerical analysis of the joints with the Boundary Element Method indicates that for the modified joints the peak reaction on the interface drops greatly but the peak stress does not rise at both the contacting and non-contacting interface in elastic bodies. Comparative experiments have been carried out. The