

压气机旋转失速特征参数的一种声学测量方法

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轴流压气机旋转失速试验的重要内容之一,是通过各种测试手段来研究失速团数目、失速团旋转角速度等旋转失速特征参数与压气机气动、几何参数之间的关系,以期对于旋转失速发生机理的理解日臻深化。与现有的方法不同,本文探索一条通过声学测量与分析达到上述目的途径。现将初步试验以及相应的分析阐述如下。

1. 试验装置和测试仪器 试验是在我校跨音压气机试验台上进行的。动力输出功率为 220.7KW,空气流量变化范围为 $0 \sim 25 \text{ kg/s}$,转速调节范围为 $8000 \sim 22000 \text{ r/min}$ 。所用试验转子外径为 355.8cm,设计转速为 16500 r/min ,相应的叶尖相对进口马赫数为 1.08。

如图 1 所示,在转子一个叶片弦长后的壁面上装有两个相距 90° 的 CH16 型传声器,另有一支 CH13 型传声器装在进气室防尘网内用以测量远场声波。由传声器输出的讯号首先进入 FDA-2 型传声放大器,然后分别进入示波器和磁带记录仪。组成了一个由传声器、传声放大器、示波器、磁带记录仪组成的声学测量系统。还包括由应变片组成的动应力监测系统以及定常气动参数和动态压力测量系统。

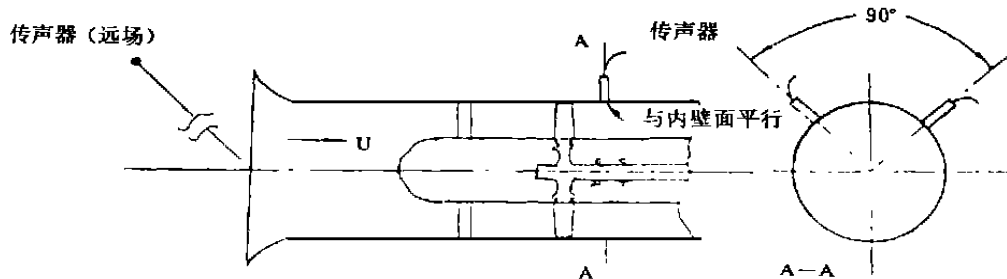


图 1 压气机声学仪器安装示意图

2. 试验结果分析 图 2 是转子转速为 $N = 12600 \text{ r/min}$,未失速条件下由两支相距 90° 的传声器在转子下游测得的时间波型。当进一步节流时,压气机出现旋转失速。图 3 是失速时在上述同样位置所测得的时间波型。比较图 2 和图 3 可以看出,旋转失速的时间波型完全不同于非失速状况下的波型,这说明失速时的时间波型已经包含了新的频率分量。由于在转子下游安装的传声器相距 90° ,因而所记录的时间波型的相位则是不一样的。根据图 3 所示的相位差,按

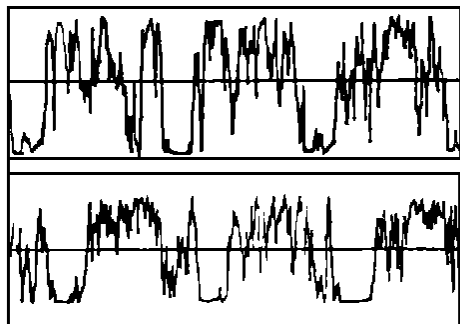


图 2 未失速时的时间波形

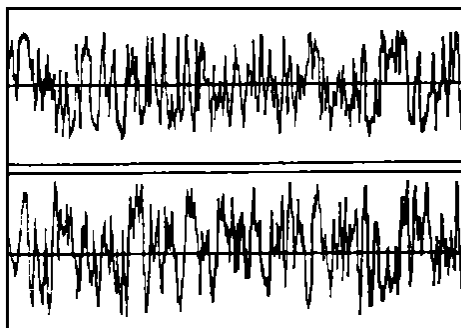


图 3 失速时的时间波形

文献 [1] 给出的方法可算出该状态下旋转失速团数目为 $B_{rs} = 1$ 。图 4、图 5 分别对应于失速和未失速状况下的声音讯号的功率谱密度。由此可以清楚地看出, 失速导致了显著的低频离散频率分量。这或许可以解释为什么失速时压气机声音会发出突变。由文献 [2] 可知, 旋转失速团与压气机叶片相互作用所产生的声音频率应为 $f = (1/2\pi)(qB_{rs}\Omega_s - nB\Omega)$, $n = 0, \pm 1, \pm 2, q = \pm 1, \pm 2$, 式中 B_{rs} 和 Ω_s 分别为失速团的个数和传播速度, 而 B 和 Ω 分别为转子叶片数和转速。对于 n, q 的不同组合, 原则上可以得到各种频率成份的声波。但是, 除非 $n = 0$, 这些频率间均不满足倍频程关系。当 $n = 0$ 时, 满足倍频程关系的声波频率是 $f = (1/2\pi)qB_{rs}\Omega_s$, $q = \pm 1, \pm 2$ 。由此可以看出, 只有旋转失速频率下的声波才满足倍频程关系。因此, 只要能在试验中发现满足倍频程关系的频率, 便可以十分明确地定出旋转失速 1 次谐波频率的大小。

这样, 若已知失速团数目, 失速团的传播速度便可以确定, 即 $\Omega_s = 2\pi f_{1rs}/B_{rs}$ 。由图 4 不难确定, 失速频率声波 1 次谐波 $f_{1rs} = 126\text{Hz}$, 相应的谐波分量是 $f_{2rs} = 252\text{Hz}$, $f_{3rs} = 382\text{Hz}$ 。这样, 便可以求出转速为 $N = 12600\text{r/min}$ 失速时失速团的传播速度 $\Omega_s = 2f_{1rs}/B_{rs} = 791.2\text{rad/s}$, 而相应的传播速率为 $K' = \Omega_s/\Omega = 0.60$ 。

3. 结束语 用我们所提出的声学方法获取旋转失速特征参数的途径是可行的。这是一种非接触的测量方法, 具有对所测量的流场不产生干扰的优点。把此种非接触测量方法用于整台发动机故障现场监测, 有待进一步深入。

参 考 文 献

- [1] Costilow, E. L. and Huppert, M. G., "Rotating-Stall Characteristics of A Rotor with High Hup-tip Radius Ratio", NACA TN-3518, 1955.
- [2] 孙晓峰, "航空动力装置某些气动声学问题的研究", 博士学位论文, 北京航空航天大学, 1988 年。

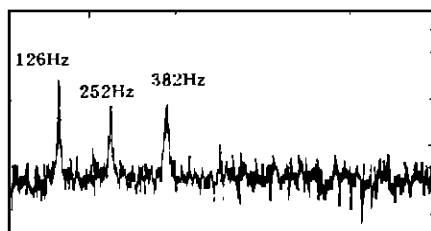


图 4 失速状态下的声音频谱(0—1000Hz)

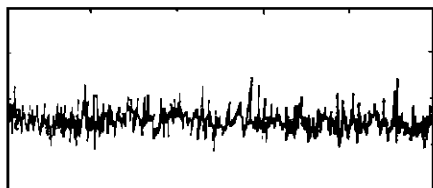


图 5 未失速状态下的声音频谱(0—100Hz)

turbulence generator, in result the examinational pattern was successfully simulated. Practice of its application proves that the simulation poles are simpler, less consumptive in energy and man-hour and more accurate in simulation than the traditional distortion screen.

FUZZY CLUSTERING ANALYSIS OF GAS TURBINE ENGINE MISSION PROFILES

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ABSTRACT

In order obtain engine mission profiles from a vast amount of flight test, the fuzzy matrix of the membership function of engine mission profile samples is established according to the theory of fuzzy sets and boolean algebra behaviours. The fuzzy matrix is examined by using square method for meeting the equivalent conditions. When it meets equivalent conditions, the dynamic clustering is carried out by selecting various threshold values. The clustering analysis of the mission profiles for an actual engine has been completed by the complicated and enormous fuzzy calculation based on statistical data of the engine loads measured in flight test. The clustering method of three parameters (flight altitude, Mach number and angle of throttle lever) is first employed in the clustering analysis and the results obtained are satisfactory.

AN ACOUSTIC METHOD FOR MEASURING CHARACTERISTICS OF ROTATING STALL IN A COMPRESSOR

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ABSTRACT

According to analysis of the characteristics of frequency and propagation of the sound generated by the rotating stall, an acoustic measuring method is developed, in which the characteristic parameters, such as the number and propagation speed of stall cells, are measured. Compared with existing methods, this method is a untouched measurement so as to avoid not disturb ance of the flow field . The primary experimental results obtained on a transonic axial-flow compressor facility demonstrate the feasibility of this method.

EXPERIMENTAL INVESTIGATION ON JET NOISE

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ABSTRACT

The correlation of sound power with jet velocity is studied in this paper. It is indicated that Both Lighthill's and Lilley's formulas fit experimental data very well when Mach number of jet $Ma_j > 0.4$, but the deviation between the results obtained from the formulas and experimental data is not so negligible as $Ma_j < 0.4$. The authors propose substituting sixth power of the jet velocity instead its eighth power in the formulas. The direction sensitiveness and the frequency spectrum of jet noise have been investigated experimentally.

TECHNIQUE FOR DIGITAL PROCESSING OF COHERENT IMAGES OF PARTICLES